

Methods — Cooling Shrinkage & Shear Strain (Axisymmetric Thermo-Elastic FEM)

Purpose.

Predict bonded rubber disk shrinkage on cool-down from mold temperature T_m to room temperature T_r , and visualize the resulting shear strain field γ_{rz} in r - z .

1) Geometry & Mesh

- Axisymmetric body with options: cylinder, straight cone, or “curved cone” (two-k bump on inner/outer radii).
- Meridional mesh: structured Q4 bilinear elements ($n_r \times n_z$), nodes linearly distributed between inner/outer radii at each z .
- Axisymmetric mapping uses the current local radius R in quadrature weights ($2\pi R \cdot \det J$).

2) Material & Thermal Strain

- Small-strain, isotropic linear elasticity with near-incompressibility: given shear modulus G and $\nu=0.49 \Rightarrow$ Lamé parameters $\lambda = (2G\nu)/(1-2\nu)$, $\mu = G$.
- Uniform temperature drop $\Delta T = T_m - T_r$.
- Isotropic thermal strain vector (axisym ordering $[r_r, z_z, \theta_\theta, r_z]$) is $\epsilon_{th} = [\alpha\Delta T, \alpha\Delta T, \alpha\Delta T, 0]$.

3) Element Formulation

- Q4 axisymmetric with 2×2 Gauss integration. Shape-function gradients are mapped via the Jacobian.
- Strain-displacement matrix B includes the hoop term $\epsilon_{\theta\theta} = \Sigma(N_i \cdot u_r)/R$.
- Constitutive matrix D (axisym, linear isotropic). Element stiffness: $K_e = \int (B^T D B) \cdot (2\pi R \det J) d\xi d\eta$.
- Thermal load vector via initial-strain route: $f_{th,e} = -\int (B^T D \epsilon_{th}) \cdot (2\pi R \det J) d\xi d\eta$.

4) Boundary Conditions

- Bonded ends: All DOF fixed on $z=0$ and $z=H$ ($u_r=u_z=0$); this suppresses axial free-shrink and induces shear.
- Free ends: Only one anchor to remove rigid motion ($u_z=0$ at a corner node); the rest are free.

5) Global Solve

- Dense assembled K and f (including thermal). PCG with diagonal preconditioning solves $K u = f$.
- Nodal displacements split as u_r, u_z .

6) Shrinkage & Shear Outputs

- Dimensional shrinkage is read directly from boundary nodes: inner/outer radii after cooling $r_{inner}(z) = R_{inner} + u_r$, $r_{outer}(z) = R_{outer} + u_r$; axial contour $z_{after}(z) = z + u_z$. The plotted “AFTER” outline uses a visual scale factor for clarity.
- Shear strain γ_{rz} is computed at each element center from the displacement field: $\gamma_{rz} = \partial u_r / \partial z + \partial u_z / \partial r$, using B-matrix gradients (absolute value for coloring). Contours are mirrored about $r=0$ for the full cross-section view.
- A quick analytic status estimate (not used for the final plot) assumes uniform free shrink: $s_r = \alpha \Delta T$, $s_z = \alpha \Delta T$ (free ends) or 0 (bonded ends), and reports $|s_r - s_z|$ as a crude shear proxy.

7) Units

- Two systems: US (lb, in, °F) or SI (N, mm, °C). Lengths/G/temps are entered in the chosen system.
- CTE α is per-degree in the chosen temperature unit. When switching units, α is converted by 9/5 or 5/9 so $\alpha \Delta T$ stays consistent.

Assumptions & Notes

- Small strains; homogeneous, linear elastic solid with $\nu=0.49$ (near-incompressible). No cure kinetics or viscoelasticity.
- Uniform ΔT ; no radial/axial thermal gradients; no contact/friction modeling at walls; axisymmetric only.
- Q4 elements with $\nu \approx 0.5$ can exhibit volumetric locking; selective/reduced integration or mixed u-p would further improve fidelity.